

# Aquifer Hydraulic Conductivity Determination from Grain Size Analysis in Parts of Old Port Harcourt Township, Nigeria

H.O Nwankwoala

Department of Geology, University of Port Harcourt, Nigeria

[nwankwoala\\_ho@yahoo.com](mailto:nwankwoala_ho@yahoo.com)

## ABSTRACT

This study aims at the determination of aquifer hydraulic conductivity from grain size analysis in parts of Port Harcourt, Nigeria. Laboratory analysis of soil and aquifer materials tests were carried out on soil samples from some boreholes based on British Standards and ASTM standards. The hydraulic conductivity calculated from Hazen formula. Hydraulic conductivity (K) values for Boreholes are: Churchill Road, BH-1 ( $3.24 \times 10^{-3}$  cm/sec); Borokiri Sand fill, BH-2 ( $3.62 \times 10^{-3}$  cm/sec); Marine Base, BH-3 ( $9.61 \times 10^{-3}$  cm/sec); Aggrey Road, BH-4 ( $8.41 \times 10^{-3}$  cm/sec); Reclamation Road, BH-5 ( $2.2 \times 10^{-3}$  cm/sec) and Harold Wilson Drive, BH-6 ( $4.0 \times 10^{-3}$  cm/sec), respectively. These values are high within the typical permeability values for fine to coarse sand to gravel. The implication of high K values is that the aquifer is prolific, hence have very good water transmitting properties and can sustain withdrawal of regional importance. Based on the results obtained, all of the boreholes appraised in this work can sustain water supply needs of the rapidly urbanizing, densely populated old Port Harcourt area. Concern should only be shown in its management so that no undesirable consequence of un-harmonized withdrawal is induced.

**Keywords:** Hydraulic conductivity, Aquifers, Grain size analysis, Boreholes, Port Harcourt.

## 1. INTRODUCTION

Port Harcourt is located within latitudes  $6^{\circ} 58'$  to  $7^{\circ} 6' N$  and longitudes  $4^{\circ} 40'$  to  $4^{\circ} 55' E$  (Fig.1). It is located within the Quaternary alluvium tidal wetlands of the Niger Delta, with strong reversing tidal currents. The geology of the Niger Delta has been extensively documented by various research including Reyment (1965), Allen (1965), Short and Stauble (1967). The Niger Delta has an area of about 75000km<sup>2</sup> and the overall sedimentary sequence is dominantly composed of sand, shale and clay. The sand forms the major aquifers in the area while clay/shale forms the aquitards. The water table in the area varies with season. Generally, the water table is close to the surface, ranging from 0.6m to 1.2m below ground surface from wet season to dry season. The dominant fresh water aquifer is found within the Benin Formation which consists mostly of continental sands with clay and silt. These materials are believed to have been deposited in a continental fluvial environment. The clay units have variable thickness ranging from 1m to as much as 15m in some places. The sand and clay intercalations constitute a system of aquifers separated by aquitards given rise to a multi-aquifer system which characterize the Niger Delta (Etu-Efeotor and Odigi, 1983; Amajor, 1989a).

Although there is substantial hydraulic conductivity data on geologic materials of the Niger Delta, most of the data have been obtained from relatively shallow water wells in the upper part of the Benin Formation. Raw field data, from which hydraulic conductivities (permeability) may be deduced for the deeper Agbada Formation, are not easily accessible from the files of the multinational companies.

Like hydraulic conductivity, porosity has been evaluated for geologic materials of the Niger Delta by many researchers (Etu-Efeotor and Odigi 1983; Akpokodje 1987; 1988; Ngah 1990; Etu-Efeotor and Akpokodje, 1990; Izeze, 1990; Nwankwoala, et al., 2008). Akpokodje et al., (1996), determined porosity for these materials solely from sonic logs using the Raymer-Hurt method after correcting for compaction effects. The porosity values obtained ranged from 20-36%, and compared very well with those reported in the earlier studies. Because of the high cost of pumping tests, data is generally very scarce on pumping tests in the Niger Delta. Secondly, the general attitude of the clients is that the moment water is 'gushing' out of the well, the contractor is under pressure to demobilize from site. It hardly ever matters to them whether necessary post-installation tests are carried out or not. This is the rationale for this study.

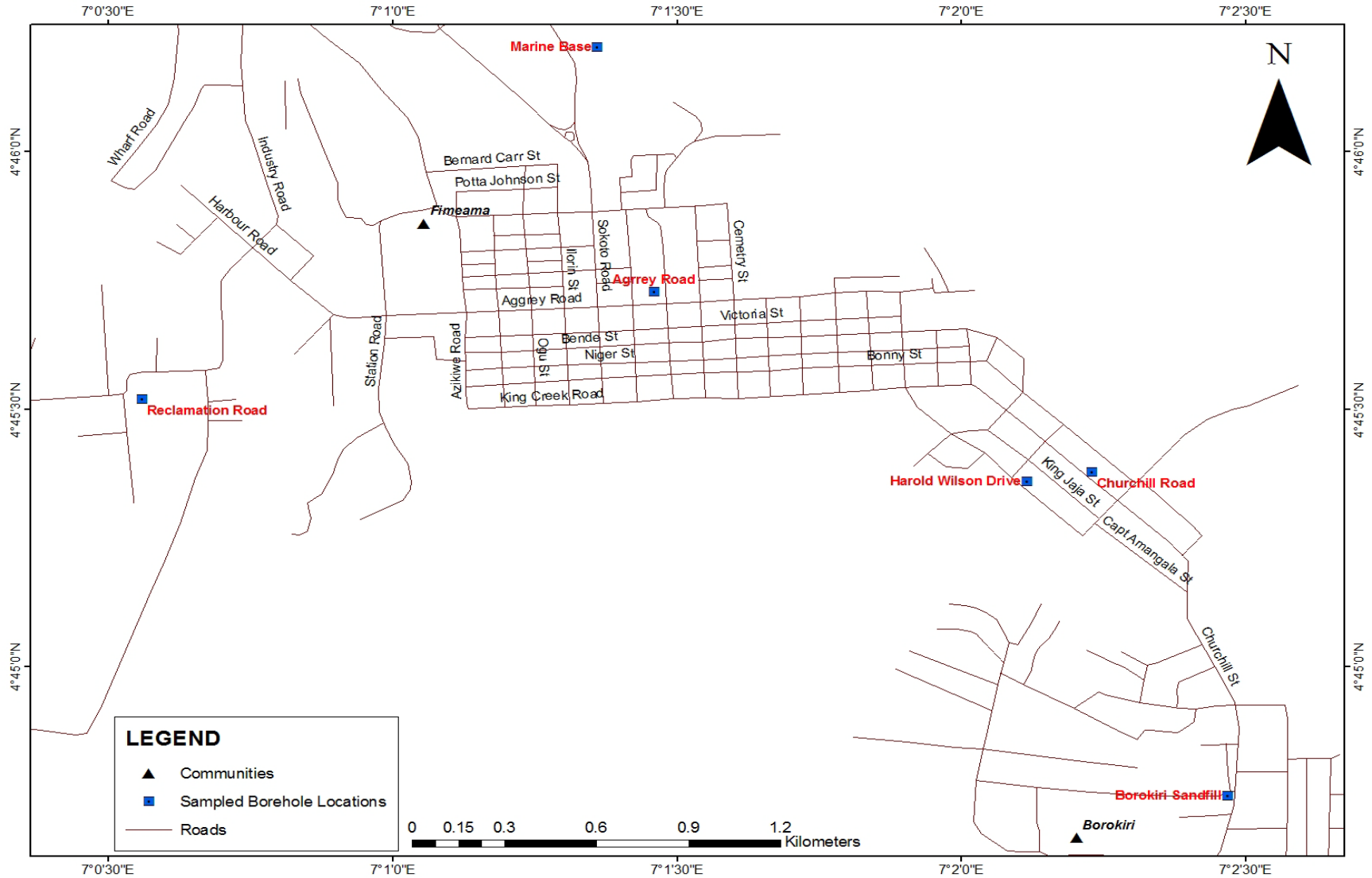


Fig 1: Map of Port Harcourt showing Study locations

## 2. METHODS OF STUDY

### 2.1 Determination of Aquifer Hydraulic Conductivity, K (Permeability)

Depending on availability of data, two methods are available for determining hydraulic conductivity of aquifer materials, namely from pumping tests and from grain size analysis of the aquifer materials. In this study, grain size analysis was used.

Laboratory Analysis of Soil and Aquifer Materials tests were also carried out on soil samples from some boreholes based on British Standards (B.S) 1377 and ASTM (1975) standards. The particle size distribution was determined by washing a known weight of oven-dried sample through ASTM sieve No.200 (0.074mm), vibrated with a shaker until no fines were retained. The hydraulic conductivity of the aquifer materials was determined from grain size analysis of the aquifer materials. The percentage passing through the successive sizes were found from the difference between the initial weight and the weight retained by each sieve. The percentage passing's were plotted against grain size to obtain grain size distribution curves. The curves were used to calculate permeability of uniform sands with the empirical formula as proposed by Hazen (1893):

$$K = Cd_{10}^2$$

where

K = hydraulic conductivity (cm/s)

C = Constant (if k is in cm/s and  $D_{10}$  in mm,  $C = 1$  (Freeze and Cherry, 1979)

$d_{10}$  = Effective diameter (mm) defined as the diameter such that 10% by weight of the porous matrix consists of grains smaller than it.

In determining the size distribution, the following procedure was followed:

- (1) Air-dry the samples;
- (2) Obtain dry representative sample and reduce it to elemental particles by disaggregating with mortar and pestle (if necessary);
- (3) Sieving the particles through a stack of sieves and weighing quantity retained on each of the sieves;
- (4) Computing the percentage passing each sieve based on the cumulative weight retained on any sieve and the total sample weight;
- (5) Plotting the percentage passing versus the sieve opening on a semi-log graph paper.

After plotting, the  $d_{10}$  value is obtained and substituted into Hazen's formula to obtain the hydraulic conductivity. However, the value of hydraulic conductivity so obtained is only an estimate.

### 2.2 Results of Sieve Analyses for Samples in the Study Area

Summary of sieve analysis result

#### Sample No. A

Location: Churchill Road (BH-1)

Sample Depth =67. 05m

Mass of sample analyzed = 78.3 grammas

Sieve Diameter (mm)	Mass Retained (g)	Mass Passing (g)	% Passing
2.000	0.0	78.3	100.0
1.000	0.4	77.9	99.5
0.425	23.5	54.4	69.5
0.250	37.9	16.5	21.1
0.150	11.2	5.3	6.8
0.063	4.8	0.5	0.6

#### Sample No. B

Location: Borokiri Sand fill (BH-2)

Sample Depth =73. 05m

Mass of sample analyzed = 81.5grammes

Sieve Diameter (mm)	Mass Retained (g)	Mass Passing (g)	% Passing
2.000	0.1	81.2	99.8
1.000	0.2	81	99.6
0.425	30.7	50.3	62.0
0.250	36.6	10.7	17.1
0.150	9.6	1.1	5.3
0.063	0.7	0.4	4.4

#### Sample No. C

Location: Marine Base (BH-3)

Sample Depth =85. 3m

Mass of sample analyzed = 36.5grammes

Sieve Diameter (mm)	Mass Retained (g)	Mass Passing (g)	% Passing
2.000	0.0	36.5	100.0
1.000	4.7	31.8	87.1
0.425	25.1	6.7	18.4
0.250	5.5	1.2	3.3
0.150	1.0	0.2	0.5
0.063	0.2	0	0

**Sample No. D**

Location: Aggrey Road (BH-4)

Sample Depth =88. 38m

Mass of sample analyzed = 44.1grammes

Sieve Diameter (mm)	Mass Retained (g)	Mass Passing(g)	% Passing
2.000	0.2	43.9	99.5
1.000	6.0	37.9	85.9
0.425	28.6	9.3	21.1
0.250	5.8	3.5	7.9
0.150	1.0	2.5	5.7
0.063	0.0	2.4	5.7

**Sample No. E**

Location: Reclamation Road (BH-5)

Sample Depth =90.10m

Mass of sample analyzed = 79.02 grammas

Sieve Diameter (mm)	Mass Retained (g)	Mass Passing (g)	% Passing
2.000	0.3	80.6	99.63
1.000	0.5	87.4	90.0
0.425	21.5	58.5	72.8
0.250	38.4	19.9	26.0
0.150	13.5	6.5	9.5
0.063	5.9	0.7	2.3

**Sample No. F**

Location: Harold Wilson Drive (BH-6)

Sample Depth =100.03m

Mass of sample analyzed = 98.07grammes

Sieve Diameter (mm)	Mass Retained (g)	Mass Passing (g)	% Passing
2.000	0.5	79.3	99.38
1.000	0.4	92	98.9
0.425	20.7	60.2	73.0
0.250	46.8	12.6	14.5
0.150	9.7	1.3	2.4
0.063	0.6	0.2	1.6

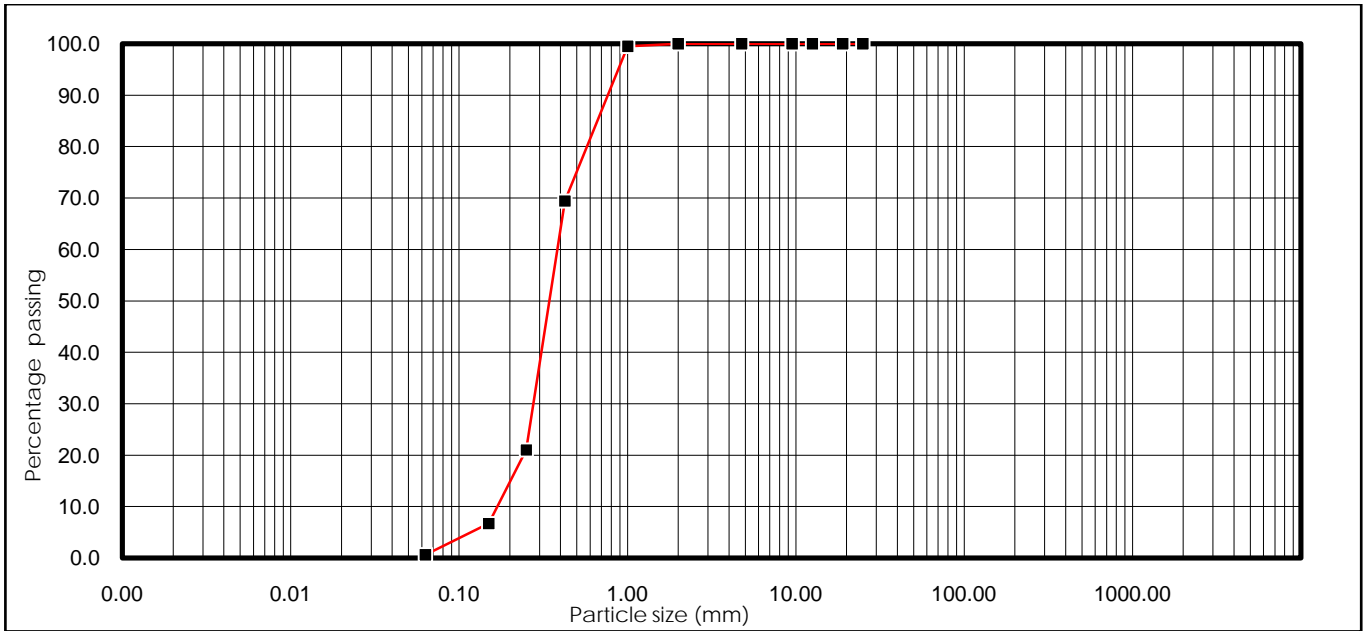
**3. RESULTS AND DISCUSSIONS**

The hydraulic conductivity calculated from Hazen formula is stated in Table 1. From Table 1, K values for Boreholes are: BH-1 ( $3.24 \times 10^{-3}$ cm/sec), BH-2 ( $3.62 \times 10^{-3}$ cm/sec), BH-3 ( $9.61 \times 10^{-3}$ cm/sec), BH-4 ( $8.41 \times 10^{-3}$ cm/sec), BH-5 ( $2.2 \times 10^{-3}$ cm/sec) and BH-6 ( $4.0 \times 10^{-3}$ cm/sec) (Table 1). These values are high within the typical permeability values for fine to coarse sand to gravel (Garg, 2005). The implication of high K values is that the aquifer is prolific.

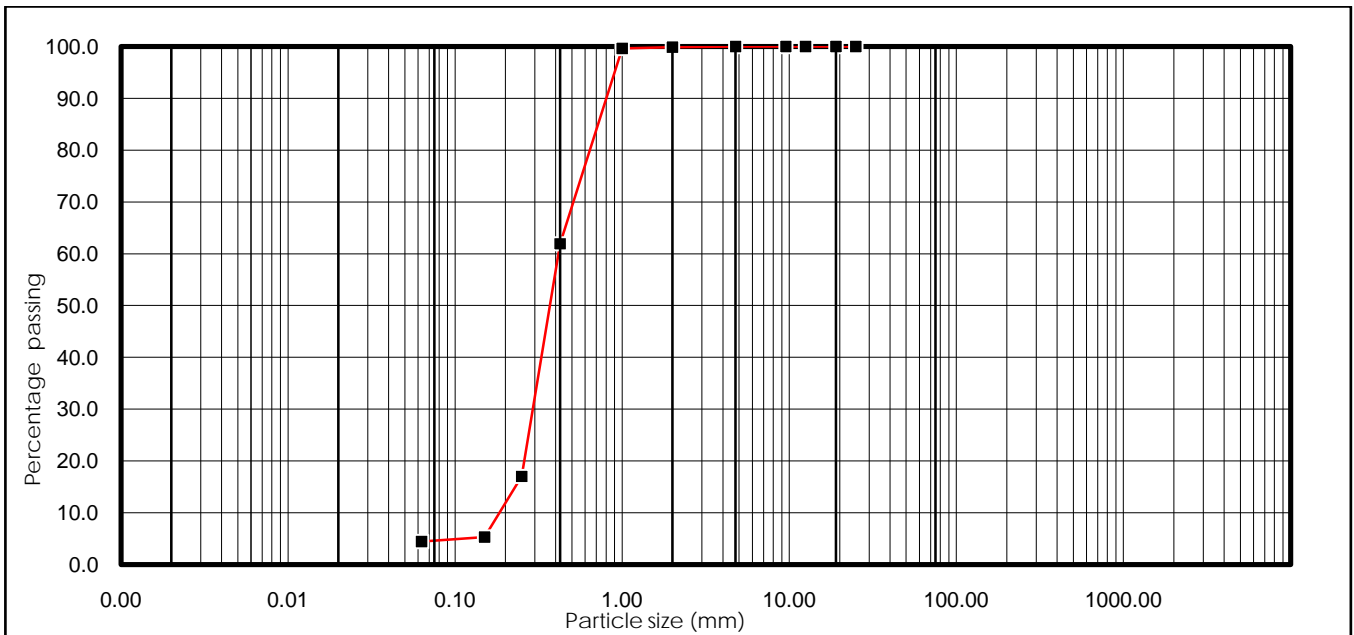
Similarly, other researchers have reported values of  $3.9 \times 10^{-4}$  to  $4.1 \times 10^{-4}$ m/s (Amajor, 1989b);  $4.2 \times 10^{-4}$  to  $4.1 \times 10^{-4}$  (Etu-Efeotor and Akpokodje, 1990); Etu-Efeotor and Odigi, 1983),  $7.0 \times 10^{-5}$  to  $1.0 \times 10^{-4}$ m/s for channel sand,  $2.0 \times 10^{-5}$  to  $5.0 \times 10^{-5}$ m/s for upper shore facies, and  $4.0 \times 10^{-6}$  to  $5.0 \times 10^{-6}$ m/s for lower shore facies (Akpokodje et al., 1996). In similar geologic materials outside the Niger Delta, hydraulic conductivities have also been estimated to range from  $4.4 \times 10^{-5}$  to  $1.5 \times 10^{-4}$ m/s (Onuoha and Mbazi, 1988), for the Ajali sandstone aquifer north of the Niger Delta.

**Table 1:** Summary of sieve analysis results

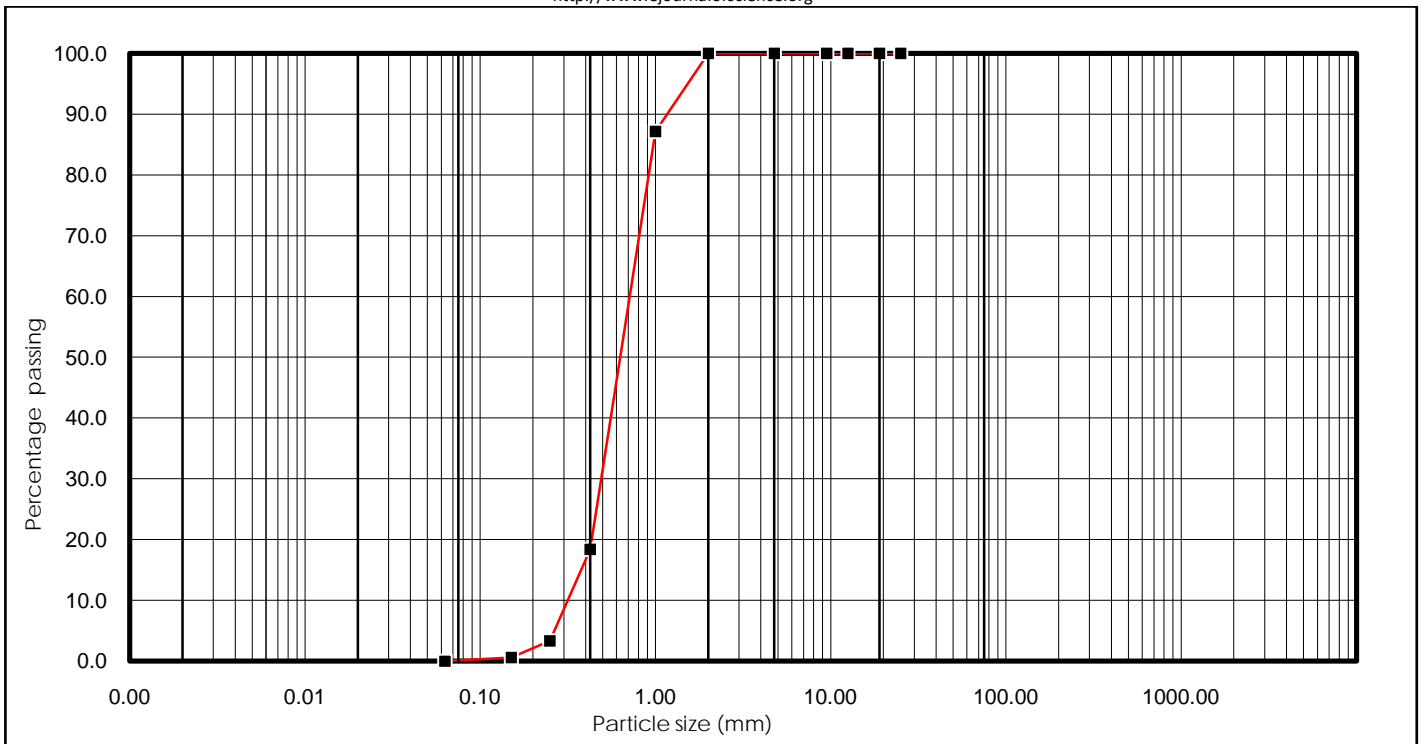
Sample No.	BH No.	Study Location	Sample Depths (m)	Medium Sand (%)	Fine (%)	Fines (%)	D <sub>10</sub> (mm)	D <sub>30</sub> (mm)	D <sub>60</sub> (mm)	C <sub>u</sub>	C <sub>c</sub>	K (cm/sec)
1	BH 1	Churchill Road	102.5	30.52	68.84	0.64	0.18	0.35	0.39	2.17	1.75	3.24 x 10 <sup>-3</sup>
2	BH 2	Borokiri Sand fill	90.3	38.04	57.55	4.42	0.19	0.295	0.41	2.16	1.12	3.61 x 10 <sup>-3</sup>
3	BH 3	Marine Base	87.2	81.64	18.36	0.00	0.31	0.5	0.7	2.26	1.15	9.61 x 10 <sup>-3</sup>
4	BH 4	Aggrey Road	96.4	78.91	15.42	5.67	0.29	0.49	0.7	2.41	1.18	8.41 x 10 <sup>-3</sup>
5	B H 5	Reclamation Road	90.10	27.20	70.49	2.32	0.15	0.27	0.38	2.53	1.28	2.2 x 10 <sup>-3</sup>
6	B H 6	Harold Wilson Drive	100.3	27.00	71.38	1.63	0.2	0.29	0.38	1.90	1.11	4.0 x 10 <sup>-3</sup>



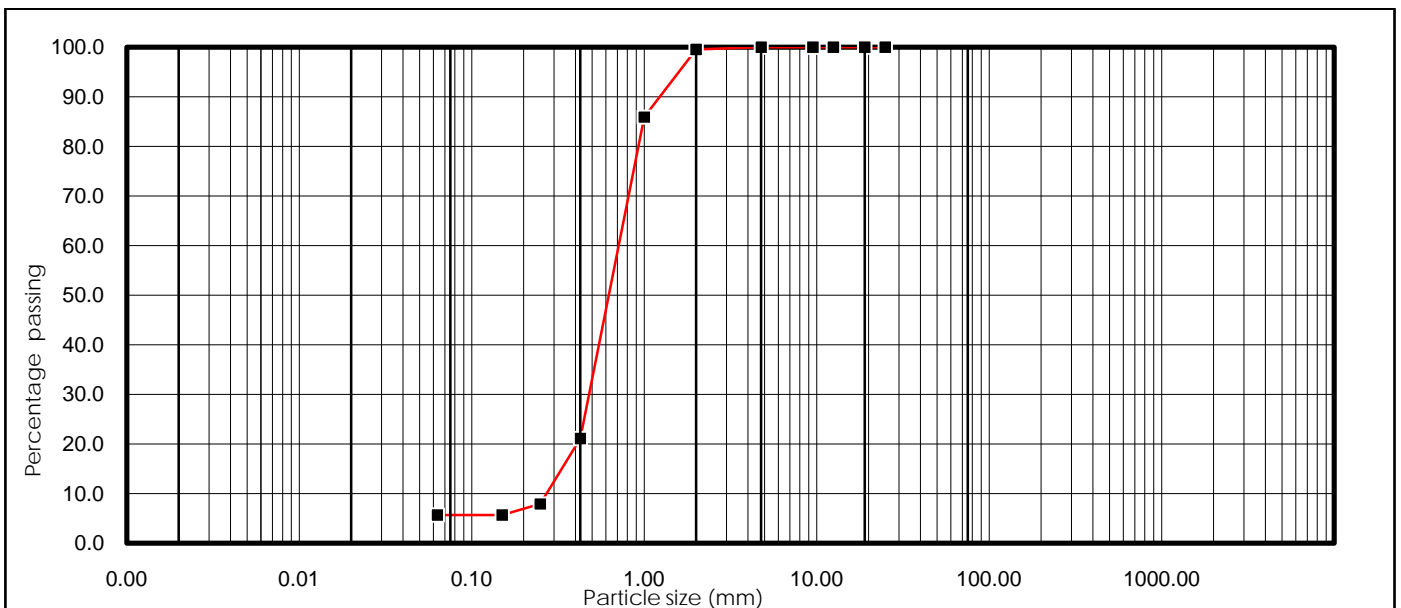
**Fig 2:** Grain size distribution curve of BH 1 @ 67.05m



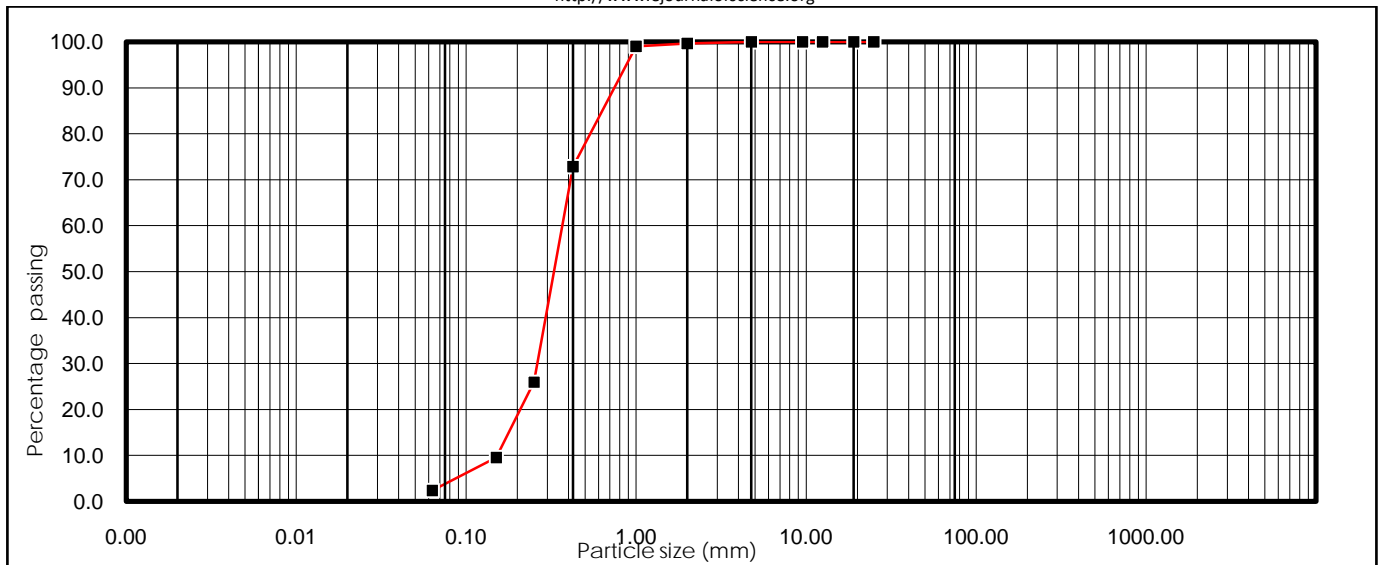
**Fig 3:** Grain size distribution curve of BH 2 @ 73.05m



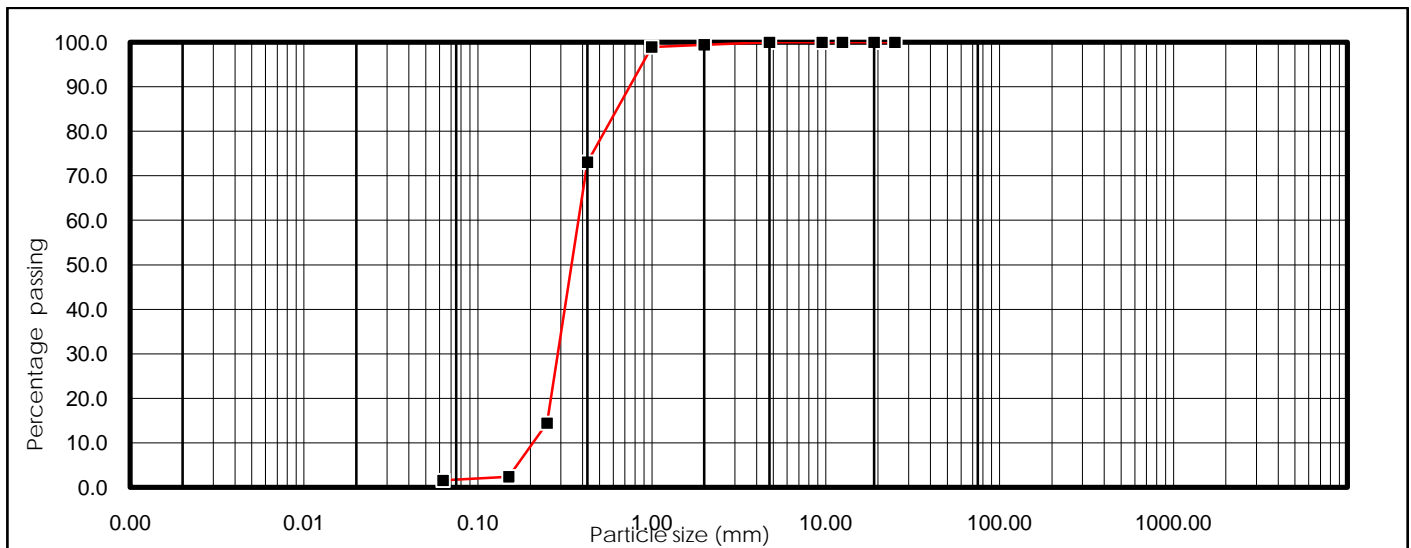
**Fig 4:** Grain size distribution curve of BH 3 @ 85.30m



**Fig 5:** Grain size distribution curve of BH 4 @ 88.38m



**Fig 6:** Grain size distribution curve of BH 5 @ 90.10m



**Fig 7:** Grain size distribution curve of BH 6 @ 100.03m

#### 4. CONCLUSION

This study reveals that the hydraulic conductivity (K) values for Boreholes studied includes: Churchill Road, BH-1 ( $3.24 \times 10^{-3}$  cm/sec); Borokiri Sand fill, BH-2 ( $3.62 \times 10^{-3}$  cm/sec); Marine Base, BH-3 ( $9.61 \times 10^{-3}$  cm/sec); Aggrey Road, BH-4 ( $8.41 \times 10^{-3}$  cm/sec); Reclamation Road, BH-5 ( $2.2 \times 10^{-3}$  cm/sec) and Harold Wilson Drive, BH-6 ( $4.0 \times 10^{-3}$  cm/sec), respectively. These values are high within the typical permeability values for fine to

coarse sand to gravel. This shows the capability of the aquifer in transmitting enough water to boreholes. Earlier estimates of hydraulic parameters for boreholes in the Niger Delta (Allen, 1992, Etu-Effector, 2000) are in general agreement with the results from this study. It is recommended that detailed hydraulic conductivity studies using both pumping test and grain size analysis be carried in the Niger Delta.



**REFERENCES**

- [1] Akpokodje, E.G. (1987): Engineering geological characteristics and Classification of the Major Superficial Soils of the Niger Delta. *Engineering Geology*, 23 Vol. 193 – 211pp.
- [2] Akpokodje, E.G., Etu-Efeotor, J.O., & Mbeledogu, I.U (1996) "A study of environmental effects of deep subsurface injection of drilling waste on water resources of the Niger Delta" CORDEC, University of Port Harcourt, Choba, Port Harcourt, Nigeria.
- [3] Allen, J. R. C (1965). Late Quaternary Niger Delta and Adjacent Area; Sedimentary Environment and Lithofacies, AAPG Bulletin, Vol. 49, 547-600pp
- [4] Allen, R.O (1992). Iron and chloride groundwater contaminants in Rivers State: geographic and stratigraphic distribution and genesis. Unpublished M.Sc Thesis, University of Port Harcourt.
- [5] Amajor, L. C. (1989a). Geological appraisal of groundwater exploration in the Eastern Niger Delta, In; C. O. Ofoegbu (Ed.), *Groundwater and mineral resources of Nigeria*; Brauschweig/Weisbaden, Friedr Vieweg an Sihh, pp. 85-100.
- [6] Amajor, L.C (1989b). Aquifers in the Benin Formation (Miocene- Recent) eastern Niger Delta, Nigeria: Lithostratigraphy, Hydraulics, and Water Quality. *Environmental Geology, Water Science*, Vol.17(2):85 – 101
- [7] American Society for Testing Materials (ASTM) (1975). Special procedure for testing soil and rocks for engineering purposes. Technical Publication. No.475 5<sup>th</sup> Edition
- [8] British Standards Institute. BS 1377 (1975). Methods of test for soils for engineering purposes. British Standard Institution (BSI), London.
- [9] Etu- Efeotor, J.O and Akpokodje, G.E(1990). Aquifer systems of the Niger Delta. *Journal of Mining and Geology*, Vol.2, No.2,pp264- 266
- [10] Etu-Efeotor, J. O. and Odigi, M. I (1983). Water supply problems in the Eastern Niger Delta. *Journal of Mining and Geology*, Vol.20, No.1 &2, pp182 – 192.
- [11] Etu-Efeotor, J.O (2000). Hydraulic characteristics of the aquifers within the Oligocene-Recent Coastal Plain Sands in parts of Southern Nigeria. *Global Journal of Pure and Applied Sciences*, Vol.6(1):107 – 115
- [12] Freeze, R.A and Cherry, J.A (1979). *Groundwater*, Prentice Hall, Englewood Cliffs, New Jersey, pp80 – 87.
- [13] Garg, S.K (2005). Soil mechanics and foundation engineering; Recent developments onshore and offshore. Proc. 7<sup>th</sup> World Petroleum Congress, Vol.2, pp 195 – 209
- [14] Hazen, A (1983). Some physical properties of sands and gravels. Mass State Board Health, 24<sup>th</sup> Annual Report.
- [15] Izeze, I.A (1990). Aquifer characterization of the Coastal [14]Plain Sands of Nigeria. Unpublished M.Sc Thesis, University of Port Harcourt, 130p
- [16] Ngah, S.A (1990). Groundwater Resource development in [15]the Niger Delta: Problems and Prospects. Proceedings of the 6<sup>th</sup> International Conference on Applied and Engineering Hydrology, Amsterdam, The Netherlands, pp80 – 90.
- [17] Nwankwoala, H.O; Abam,T.K.S; Ede,P.N, Teme, S.C and [16]Udom,G.J (2008). Estimates of aquifer hydraulic properties from pumping test data: A case study of Port Harcourt and environs. *Water Resources Journal*, Vol.18, pp25 – 31
- [18] Onuoha, K.M and Mbazi, F.C.C (1988). Aquifer transmissivity from electrical sounding data: the case of Ajali Sandstone aquifers, Southwest of Enugu, Nigeria. In Ofoegbu, C.O (Ed.) *Groundwater and Mineral Resources of Nigeria*, Vieweg-Verlag, 17 – 30
- [19] Reyment, R.A (1965). Aspects of Geology of Nigeria, University of Ibadan Press, Nigeria, pp52 – 54.
- [20] Short, K.C and Stauble, A.J (1967). Outline of the Geology of the Niger Delta, AAPG Bulletin, Vol.51, pp761 – 769.

**ABOUT THE AUTHOR**

Nwankwoala, Hycienth Ogunka is a Lecturer I in the Department of Geology, University of Port Harcourt, Nigeria. He holds a B.Sc Degree in Geology, from the University of Port Harcourt and an M.Phil Degree in Environmental Management from the Rivers State University of Science and Technology, Port Harcourt,

<http://www.ejournalofscience.org>

Nigeria. His major areas of interest are Applied geophysics, hydro geochemistry, water quality  
Hydrogeology, Environmental Hydrogeology, Hydro management, geochemical modeling and pollution studies.